

## PPII – equations being at students' disposal for the exam

Any axisymmetric body

$$\varepsilon_r = \frac{du}{dr} \quad \varepsilon_t = \frac{u}{r} \quad \varepsilon_z = \frac{dw}{dz} \quad u = r\varepsilon_t = \frac{r}{E} [\sigma_t - \mu(\sigma_r + \sigma_z)]$$

Cylindrical vessel

$$\sigma_r = A - \frac{B}{r^2} \quad \sigma_t = A + \frac{B}{r^2}$$

Rotating disc

$$\sigma_r = A - \frac{B}{r^2} - \frac{3+\mu}{8} \rho \omega^2 r^2 \quad \sigma_t = A + \frac{B}{r^2} - \frac{1+3\mu}{8} \rho \omega^2 r^2$$

Axisymmetric plate

$$\frac{d^2 v}{dr^2} + \frac{1}{r} \frac{dv}{dr} - \frac{1}{r^2} v = -\frac{t(r)}{B} \quad \approx \quad \frac{d}{dr} \left[ \frac{1}{r} \frac{d}{dr} (rv) \right] = -\frac{t(r)}{B}$$

$$v(r) = c_1 r + \frac{c_2}{r} + v_p \quad w(r) = c_1 \frac{r^2}{2} + c_2 \ln r + w_p + c_3$$

$$u = -z v \quad v = t g v = \frac{dw}{dr}$$

$$m_r = -B \left[ \frac{dv}{dr} + \mu \frac{v}{r} \right] \quad m_t = -B \left[ \frac{v}{r} + \mu \frac{dv}{dr} \right] \quad B = \frac{Eh^3}{12(1-\mu^2)}$$

$$\sigma_r = \frac{12m_r}{h^3} z \quad \sigma_{r \max} = \pm 6m_r / h^2$$

$$\sigma_t = \frac{12m_t}{h^3} z \quad \sigma_{t \max} = \pm 6m_t / h^2$$

Membrane shell

$$\frac{\sigma_t}{r_t} + \frac{\sigma_m}{r_m} = \frac{p}{h} \quad 2\pi r h \sigma_m \sin \varphi_m - F_z + F_{rz} = 0$$

### Momentum shell

$$u = e^{-\beta z} (c_1 \sin \beta z + c_2 \cos \beta z) + e^{\beta z} (c_3 \sin \beta z + c_4 \cos \beta z) + u_{part}$$

$$u_{part} = \frac{r^2}{Eh} \left[ p - \frac{\mu}{r} n_z \right] \quad \beta = \sqrt[4]{\frac{3(1-\mu^2)}{r^2 h^2}} \quad l_0 = 4 / \beta \cong 3\sqrt{rh}$$

$$n_z = \frac{Eh}{1-\mu^2} \left[ \frac{dw}{dz} + \mu \frac{u}{r} \right] \quad n_t = \frac{Eh}{1-\mu^2} \left[ \frac{u}{r} + \mu \frac{dw}{dz} \right] \quad v = \frac{du}{dz}$$

$$m_z = -B \frac{d^2 u}{dz^2} \quad m_t = -\mu B \frac{d^2 u}{dz^2} = \mu m_z \quad t = -B \frac{d^3 u}{dz^3}$$

$$B = \frac{Eh^3}{12(1-\mu^2)} \quad n_t = \mu n_z + Eh \frac{u}{r}$$

$$\sigma_{t \max} = \frac{n_t}{h} \pm \frac{6m_t}{h^2} \quad \sigma_{z \max} = \frac{n_z}{h} \pm \frac{6m_z}{h^2}$$

### Factor of safety for cyclic loading

$$k_C = \frac{\sigma_C^*}{\frac{\sigma_C^*}{\sigma_C} \psi_\sigma \sigma_m + \sigma_a} \cong \frac{\sigma_C^*}{\sigma_{ae}} \quad \sigma_C^* = \sigma_C \frac{v\eta}{\beta} \quad k_C = \frac{k_{C\sigma} \cdot k_{C\tau}}{\sqrt{k_{C\sigma}^2 + k_{C\tau}^2}}$$

### Fracture mechanics (LEFM)

$$\sigma_{ij} = \frac{1}{\sqrt{2\pi r}} \left[ K_I \cdot f_{ij}^I(\varphi) + K_{II} \cdot f_{ij}^{II}(\varphi) + K_{III} \cdot f_{ij}^{III}(\varphi) \right]$$

$$K_I = \sigma \sqrt{\pi a} \cdot f\left(\frac{a}{b}\right) \quad r_k = \frac{\alpha}{\pi} \left( \frac{K_I}{R_e} \right)^2$$

$$a_c \cong \left( \frac{K_{IC}}{\sigma} \right)^2 \cdot \frac{1}{\pi} \quad v_T = \frac{da}{dN} = c(\Delta K_I)^m \quad \Delta N = \frac{2 \left( a_f^{1-\frac{m}{2}} - a_0^{1-\frac{m}{2}} \right)}{c \Delta \sigma^m \pi^{\frac{m}{2}} (2-m)}$$

SCHEMA	VZTAH PRO K	S PŘESNOSTÍ PLATÍ PRO
	$K_I = 6\sqrt{a} \frac{1 - 0,5(\frac{a}{b}) + 0,37(\frac{a}{b})^2 - 0,044(\frac{a}{b})^3}{\sqrt{1 - \frac{a}{b}}}$ $K_{II} = K_{III} = 0$	0,3% PRO JAKÉKOLIV $\frac{a}{b}$ $a < b$ $\frac{h}{b} \geq 3$
	$K_I = 6\sqrt{a} \frac{1,122 - 0,561(\frac{a}{b}) - 0,205(\frac{a}{b})^2 + 0,471(\frac{a}{b})^3 - 0,19(\frac{a}{b})^4}{\sqrt{1 - \frac{a}{b}}}$ $K_{II} = K_{III} = 0$	0,5% PRO JAKÉKOLIV $\frac{a}{b}$ $a < b$ $\frac{h}{b} \geq 2,75$
	$K_I = 6\sqrt{a} [1,12 - 0,231(\frac{a}{b}) + 10,55(\frac{a}{b})^2 - 21,72(\frac{a}{b})^3 + 30,39(\frac{a}{b})^4]$ $K_{II} = K_{III} = 0$	0,5% PRO $\frac{a}{b} \leq 0,6$ $a < b$ $\frac{h}{b} \geq 1$
	$\sigma = \frac{6M_o}{tb^2}$ $K_I = 6\sqrt{a} [1,122 - 1,4(\frac{a}{b}) + 7,33(\frac{a}{b})^2 - 13,08(\frac{a}{b})^3 + 14,0(\frac{a}{b})^4]$ $K_{II} = K_{III} = 0$	0,2% PRO $\frac{a}{b} \leq 0,5$ $a < b$ $\frac{h}{b} \geq 2$
	$\sigma = \frac{6M_o}{tb^2} \quad (M_o = \frac{Fs}{4})$ $K_I = 6\sqrt{a} [1,107 - 2,12(\frac{a}{b}) + 7,71(\frac{a}{b})^2 - 13,55(\frac{a}{b})^3 + 14,25(\frac{a}{b})^4]$ $K_{II} = K_{III} = 0$	0,2% PRO $\frac{a}{b} \leq 0,6$ $\frac{a}{b} = 8$
	$K_I = 1,1215\sigma\sqrt{a}$ $K_{II} = 1,1215\alpha\sqrt{a}$ $K_{III} = \alpha_2\sqrt{a}$	$K_I, K_{II}$ PRAKTICKY PŘESNĚ $K_{III}$ PŘESNĚ
	$K_I = 3,975 \frac{M_o}{\alpha a \sqrt{a}}$ $K_{II} = K_{III} = 0$	DO 0,1%
	$\sigma = \frac{3M_o}{2tb^2} \quad K_{II} = K_{III} = 0$ $\sigma_N = \frac{3M_o}{E2(b-a)^2} = \frac{\sigma}{1 - (\frac{a}{b})^2}$ $K_I = \sigma\sqrt{a} \cdot f_1(\frac{a}{b}) = \sigma_N\sqrt{a} f_2(\frac{a}{b})$ $f_1(\frac{a}{b}) = \frac{4}{3\sqrt{1 - (\frac{a}{b})^2}} \{ 1 + \frac{1}{2}(\frac{a}{b}) + \frac{3}{8}(\frac{a}{b})^2 + \frac{5}{16}(\frac{a}{b})^3 \} - 0,47(\frac{a}{b})^4 + 0,663(\frac{a}{b})^5$ $f_2(\frac{a}{b}) = (1 - \frac{a}{b})^2 F_1(\frac{a}{b})$	LEPŠÍ NEŽ 1% $a < b$