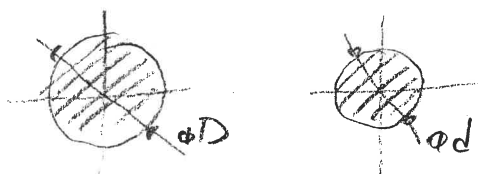
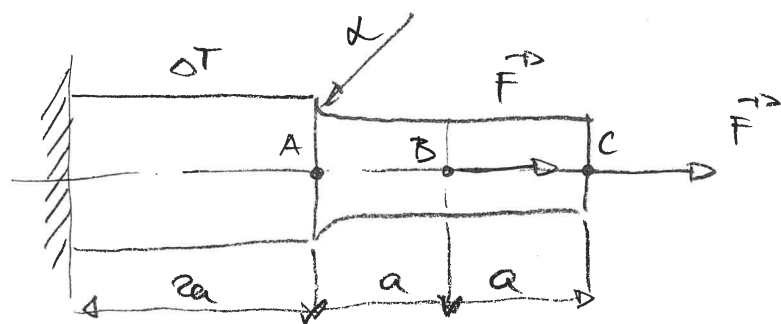


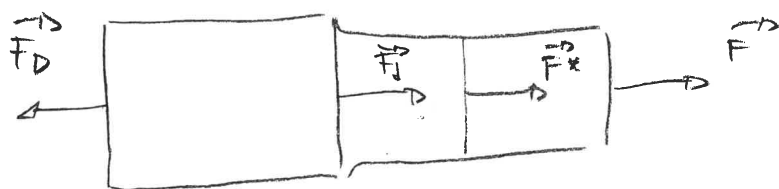
Př: Stanovte bezpečnost křes pružnosti a posunů při čer<sup>o</sup> A, B, C.



$$\begin{aligned} F &= 12 \text{ N} \\ a &= 500 \text{ mm} \\ d &= 20 \text{ mm} \\ D &= 30 \text{ mm} \\ E &= 2.1 \cdot 10^5 \text{ MPa} \\ \alpha_T &= 12.5 \cdot 10^{-6} \text{ K}^{-1} \\ \Delta T &= 50 \text{ }^\circ\text{C} \\ \alpha &= 1.3 \\ \sigma_k &= 300 \text{ MPa} \end{aligned}$$

### 1. Úplně uvolněn

$$|\vec{F}_d| = 0 \quad |\vec{F}^*| = F$$

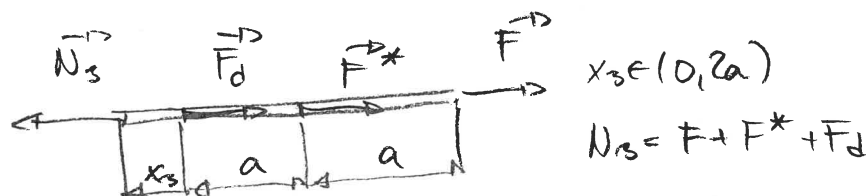
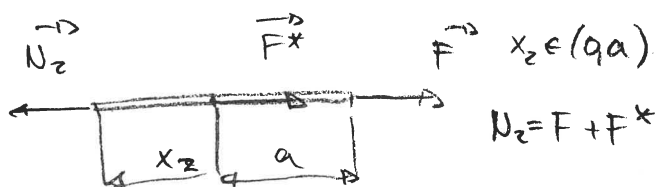
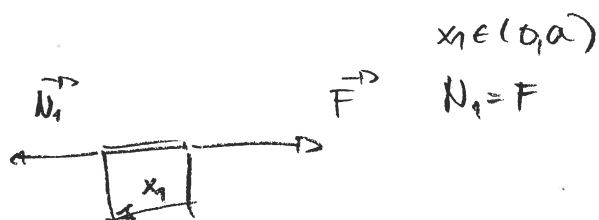


### 2. Stat. uvolněn

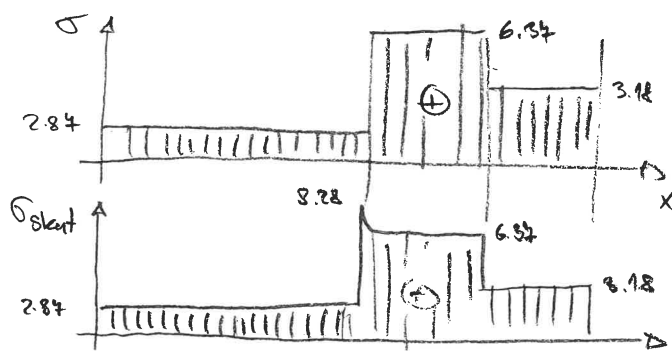
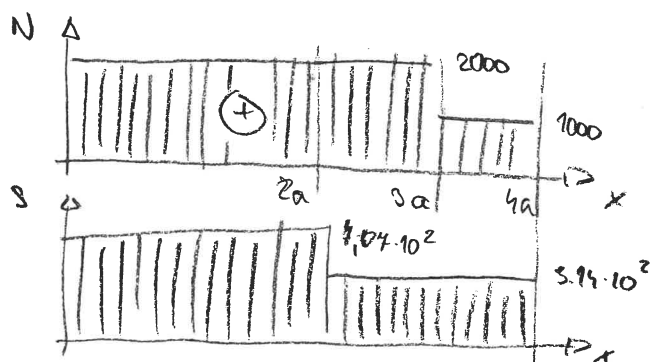
$$NP = \{ F_d \}$$

$$\left. \begin{aligned} \mu &= 1 \\ \nu &= 1 \end{aligned} \right\} s = \mu - \nu = 0 \leftarrow \text{úloha stat. uvolně}$$

### 3. UV



### 4. Řešení



$$\sigma_{skint} = \alpha \cdot \frac{N_2}{S_1} = 1.3 \cdot \frac{2000}{\frac{\pi \cdot 20^2}{4}} = 8.28 \text{ MPa}$$

$$k = \frac{\sigma_k}{\sigma_{skint}} = \frac{300}{8.28} = \underline{\underline{36.2}}$$

$$\begin{aligned} u_A = \frac{\partial W}{\partial F_d} &= \int_0^a \frac{N_1}{ES_1} \frac{\partial N_1}{\partial F_d} dx_1 + \int_0^a \frac{N_2}{ES_1} \frac{\partial N_2}{\partial F_d} dx_2 + \int_0^{2a} \frac{N_3}{ES_2} \frac{\partial N_3}{\partial F_d} dx_3 + \Delta T \alpha_T \cdot 2a = \\ &= \frac{N_1 \cdot a}{ES_1} \frac{\partial N_1}{\partial F_d} + \frac{N_2 \cdot a}{ES_1} \frac{\partial N_2}{\partial F_d} + \frac{N_3 \cdot 2a}{ES_2} \frac{\partial N_3}{\partial F_d} + \Delta T \alpha_T \cdot 2a = \frac{F \cdot a}{ES_1} \cdot 0 + \frac{2Fa}{ES_1} \cdot 0 + \\ &+ \frac{2Fa}{ES_2} \cdot 1 + \Delta T \alpha_T \cdot 2a = \frac{4Fa}{ES_2} + \Delta T \alpha_T \cdot 2a \end{aligned}$$

$$\begin{aligned} u_B = \frac{\partial W}{\partial F^*} &= \frac{N_1 \cdot a}{ES_1} \frac{\partial N_1}{\partial F^*} + \frac{N_2 \cdot a}{ES_1} \frac{\partial N_2}{\partial F^*} + \frac{N_3 \cdot 2a}{ES_2} \frac{\partial N_3}{\partial F^*} + \Delta T \alpha_T \cdot 2a = \frac{F \cdot a}{ES_1} \cdot 0 + \\ &+ \frac{2Fa}{ES_1} \cdot 1 + \frac{2Fa}{ES_2} \cdot 1 + \Delta T \alpha_T \cdot 2a = \frac{2Fa}{E} \left( \frac{1}{S_1} + \frac{2}{S_2} \right) + \Delta T \alpha_T \cdot 2a \end{aligned}$$

$$\begin{aligned} u_C = \frac{\partial W}{\partial F} &= \frac{N_1 \cdot a}{ES_1} \frac{\partial N_1}{\partial F} + \frac{N_2 \cdot a}{ES_1} \frac{\partial N_2}{\partial F} + \frac{N_3 \cdot 2a}{ES_2} \frac{\partial N_3}{\partial F} + \Delta T \alpha_T \cdot 2a = \frac{F \cdot a}{ES_1} \cdot 1 + \frac{2Fa}{ES_1} \cdot 1 + \\ &+ \frac{2Fa}{ES_2} \cdot 1 + \Delta T \alpha_T \cdot 2a = \frac{F \cdot a}{E} \left( \frac{1}{S_1} + \frac{2}{S_1} + \frac{4}{S_2} \right) + \Delta T \alpha_T \cdot 2a \end{aligned}$$

$$S_1 = 314 \text{ mm}^2, S_2 = 404 \text{ mm}^2$$

$$u_A = \frac{4 \cdot 1000 \cdot 500}{2.1 \cdot 10^5 \cdot 404} + 50 \cdot 12.5 \cdot 10^{-6} \cdot 1000 = \underline{\underline{6.38 \cdot 10^{-1} \text{ mm}}}$$

$$u_B = \frac{2 \cdot 1000 \cdot 500}{2.1 \cdot 10^5} \left( \frac{1}{314} + \frac{2}{404} \right) + 50 \cdot 12.5 \cdot 10^{-6} \cdot 1000 = \underline{\underline{6.54 \cdot 10^{-1} \text{ mm}}}$$

$$u_C = \frac{1000 \cdot 500}{2.1 \cdot 10^5} \left( \frac{1}{314} + \frac{2}{314} + \frac{4}{404} \right) + 50 \cdot 12.5 \cdot 10^{-6} \cdot 1000 = \underline{\underline{6.61 \cdot 10^{-1} \text{ mm}}}$$